Enter De 28/7/14 lec 10: Minority coveriers distribution and OIR Ideal I-V characteristics of pr jundion. Keference (R): → Einstein Relation (It holds under quasi-equilibrium) where D' > Constant associated with "diffusion" transport. (Diffusivity) "" > constant associated with "doift" transport. (Mobility) A+ T= 300K or 270C VT = KT] > Thermal voltage; VT = 0.0259 Volts Also $\frac{D_n}{\mu_n} = V_T = \frac{D_P}{\mu_P}$ $E = -\frac{d\varphi}{dx}$ • $J_{p} dm_{b} t = -2p \mu p \frac{d\psi}{dx}$ It shows, that · Jp dibbos" = - 2 Dp dp /E-field is caused by gradient of potential Transport eqn for holes: - Jp = 2pmp E - 2 Dp <u>Jp</u> drifter drifter Transport eqn for electrons: - Jn = qn un E + q Dn dn dr drift - potential gradient diffusion -> concentration gradient **INDERJIT SINGH**

Ctrl 03R For a n-segion, nno 2 Nd (Assuming complete ionization) Pro 2 nº2 (From law of mass action Law) - (°) For a p-segion Pro 2 Na (Assuming complete ionization) $\frac{n_{PO} \approx \frac{n^{\circ 2}}{Na}}{Na} - (i^{\circ})$ Equation (i) and (ii) represent total minority carrier concentration in p and n region. · PA Junction Analysis - (Goal is to explain and determine expression for I) I - The potential barouer of a pr jurction is lowered when a forward bias is applied, allowing electrons and holes to flow across the I= To exp(2V space-charge segior. - When holes flow form p-segion into n-sequen, they become excess minority carrier (holes) and are subject to the excess minosity carrier dibbusion, doibt and recombination processes. - Likewise, when electrons from n-region flow into p region they become excess conviers (electrons). 240 MDEBT INDERJIT SINGH

Ctrl PgDr · Minority Covour Distribution: (pn Junction) 04 Thermal equilibrium case: E_c . P Q^Vbi . The n-sequen contains many es in CB than P-sequens, Vb: provents fig: Conduction band enougy through this large density of es from flowing into p region. a projunction in themal · Build-in potential barrier(Vbi) equilibrium maintains equilibrium betwan cavaier distributions on either side of the junction. We know $V_{b_1^{\circ}} = \frac{KT}{q} \ln \left[\frac{NaNd}{n_1^{\circ 2}} \right] = V_T \ln \left[\frac{NaNd}{n_1^{\circ 2}} \right] \cdot \left\{ V_T = \frac{KT}{2} \right\}$ $\Rightarrow \frac{n_i^{\circ 2}}{N_e N_d} = \exp\left(-\frac{q V_{bi}}{\kappa_T}\right)$ It we assume complete ionization ie no & Nd and so npo 2 ni2 $\int n_{Po} = n_{no} \exp \left(-\frac{qV_{b}}{\kappa_{T}}\right) \qquad (1)$ Eqn O selates minority carrier concentration on p-side of the junction to the majority carrier concentration on aside of the junction in a thermal NDERJIT SINGH equilibrium. HOMIS THREAD

I Forward bias case: 05 Ebuild -in Va - Applied OD bias $P = \Theta \oplus \Omega$ $-W_P \longrightarrow K = W_0 - 1$. In for ward bias, E-field that prevented majority carriers Form crossing the space-charge segion is reduced. $n_{p} = n_{RO} \exp \left[-\frac{q \left(V_{b_{i}}^{\circ} - V_{F} \right)}{\kappa_{T}} \right]$ $= n_{no} \exp \left[-\frac{2Vb^{\circ}}{K\tau}\right] \exp \left[\frac{4Va}{K\tau}\right] - \left[\frac{K\tau}{2}\right] - \left(\overline{FromO}\right)$ $\boxed{n_{p} = n_{po} \exp \left[\frac{Va}{V\tau}\right] - (2)}$ Assuming low injection level, no (may corrier) does not change significantly. Np - to deviates from thermal-equilibrium value npo as seen in eq. (2). Equation (2) is the expression for minority councer (es) concentration at the edge of space-charge segion in p-side. -> Va Lowous potential barrier, so that maj. carrier es From a side are injected across the junction into p-side, thereby increasing minosity carrier concentration. ." There is excess minosity corriers (es) in p-region.

Similarly, we can show $P_n = P_{no} \exp\left(\frac{V_a}{v_T}\right) - 3$ Eqn 3 represents concentration of min. curriers (holes) at the edge of space-charge region in the n-side. $\Delta_{P} \leftarrow \frac{P_n(x_n)}{\varphi_r} = P_{no} \exp\left(\frac{V_a}{V_r}\right)$ np(-xp) = npo exp(Va) (An) (An) Npo - Pno Ke Space -- charge fig a): Excess minority carrier concentration at space charge edge generated by applied bias Va. . By applying a voltage Na=V= (forward-bias), we weate exans minority carriers in each segion of pr junction. $\Delta n = np = n_{po} \exp\left(\frac{V_{a}}{V_{T}}\right) \quad \& \quad \Delta p = P_{n} = P_{no} \exp\left(\frac{V_{a}}{V_{T}}\right)$ Lo Minium carrier concentrat at depletion layer edges derived assuming (varo) is applied across pn junction. -> An & AP -> symbol is used to indicate value at the depletion layer edge. Reverse Bias Case: TIL . Va -> -re (Revenue bias) > pp and pn -> reduces to zero at space - charge edges. 10

Shif 公 08R . · <u>Continuity</u> equation $\rightarrow ($ Describe's the distribution of es and holes when there is excuss current generation, secombination and carrier movement) Continuity eqn for how => $\left| \frac{\partial P}{\partial t} = -\frac{1}{q} \frac{\partial Jp}{\partial x} + \frac{G' - \delta P}{T_p} \right| - (1.1)$ Now, $\frac{\partial}{\partial t_n} = \frac{\partial P_n}{\partial t} - \frac{\partial P_{no}}{\partial t}$ From (a) t $\frac{\partial}{\partial t_n} = \frac{\partial P_n}{\partial t} - \frac{\partial P_{no}}{\partial t}$ $\frac{\partial}{\partial t_n} = \frac{\partial P_n}{\partial t} - (1,2)$ $T_p - r$ life time of Eqn (1.1) becomes, minority careiers $\frac{\partial \delta \rho_{n}}{\partial t} = -\frac{1}{2} \frac{\partial J_{p}}{\partial x} + \frac{G' - \delta \rho_{n}}{\mathcal{T}_{p}} - (1.3) \begin{cases} \frac{\partial^{2} p}{\partial x^{2}} = \frac{\partial^{2} (\delta \rho)}{\partial x^{2}} \\ \frac{\partial^{2} p}{\partial x^{2}} = \frac{\partial^{2} (\delta \rho)}{\partial x^{2}} \end{cases}$ Now, $J_p = qM_p p E - q D_p \frac{\partial P}{\partial x} - (1.4)$. $\Rightarrow \frac{\partial \delta P_{0}}{\partial t} = -\frac{1}{2} \frac{\partial}{\partial x} \left[-2 D_{P} \frac{\partial P}{\partial x} + 4\mu P PE \right] + G' - \frac{\partial P_{0}}{\mathcal{T}_{P}} \\ \frac{\partial \delta P_{0}}{\partial t} = D_{P} \frac{\partial^{2} (\delta P_{0})^{A}}{\partial x^{2}} - \mu_{P} \cdot E \frac{\partial P}{\partial x} + G' - \frac{\partial P_{0}}{\mathcal{T}_{P}} \\ \frac{\partial \delta P}{\partial t} = \frac{\partial P}{\partial x^{2}} \frac{\partial^{2} (\delta P_{0})^{A}}{\partial x^{2}} - \mu_{P} \cdot E \frac{\partial P}{\partial x} + G' - \frac{\partial P_{0}}{\mathcal{T}_{P}} \\ \frac{\partial P}{\partial x} = \frac{\partial P}{\partial x^{2}} + \frac{\partial P}{\partial x} + \frac{\partial P}{\mathcal{T}_{P}} + \frac{\partial P}{\mathcal{T}_{P}} \\ \frac{\partial P}{\partial x} = \frac{\partial P}{\partial x^{2}} + \frac{\partial P}{\partial x} + \frac{\partial P}{\mathcal{T}_{P}} + \frac{\partial P}{\mathcal{T}_{P}} \\ \frac{\partial P}{\partial x} = \frac{\partial P}{\partial x} + \frac{\partial P}{\partial x} + \frac{\partial P}{\mathcal{T}_{P}} + \frac{\partial P}{\mathcal{T}_{P$ Ambipoler Transport eq " for excess minor ty (1.4) Ambipoler Transport eq " for excess minor ty (1.4)

This page is just for explaining how we got the Ambipolar transport circuit

M investy Carvier Distribution (in p and n region)
A Minority Carvier Distribution (in p and n region)
A Multiplex transport on Fr excess monthly carvies (holds)
in n-region is

$$\frac{\partial (dra)}{\partial t} = Dp \frac{\partial^2 (dra)}{\partial x^2} - \mu p E \frac{\partial (dra)}{\partial x} + G^{-1} - \frac{Gra}{Dp} - (0)$$
where, $dra = Pa - Paao is the excess minority carvier
holes concentration.
In equilibrium, when no veltage is applied (E=0)
in n-region for x >>xa, the net change of holes
concentration ($\frac{\partial (dra)}{\partial t} = 0$
:... Equation (0) reduces to,

$$\frac{d^2 (dra)}{dx^2} - \frac{Gra}{Lp^2} = 0 - (x = xa) - (2)$$
where, $[Lp^2 = Dp Tp]$
Similarity, for p-region,

$$\frac{d^2 (drap)}{dx^2} - \frac{drap}{Lax} = 0 - (x = xp) + (3)$$
Where, $[Lp^2 = Dn Ta]$
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Boundary conditions for total minority carries concentrations are

$$4u \begin{bmatrix} Pn(2n) = Pn_0 \exp\left(\frac{Vn}{VT}\right) \\ Pn(-xp) = n_p \exp\left(\frac{Vn}{VT}\right) \\ 4b \begin{bmatrix} Pn(2n-y_0) = Pn_0 \\ Pn(-xp) = n_p \\ 4b \begin{bmatrix} Pn(2n-y_0) = Pn_0 \\ Pn(-x-y_0) = Pn_0 \\ Pn(-$$

12 Similarly, For (x ≤ xp), = npo $\exp\left(\frac{Va}{Vr}\right) \exp\left(\frac{\pi p + \pi}{Ln}\right)$ --- for (oc < xp) where, $n_{p} = n_{po} \exp\left(\frac{V_{\alpha}}{V_{T}}\right)$ From eqn (9) and (10), we interpretate ". The minority carrier conast sation decay exponentially with distance away from the junction to their thermal-equilibrium values !! (Assuming Wn>>Lp and Wp>>Ln) ie Both norgion end posegion lengths are long compared to minority carrier dibbusion lengths (Lp and Lp) $V P_n(xn) = P_{n_0} \exp\left(\frac{V_a}{V_r}\right)$ $\bigcap p(-xp) = \bigcap po \exp\left(\frac{V_{a}}{V_{T}}\right)$ fig(c) Distribut $\bigvee \int_{Pn} (x) = P_n \exp\left(\frac{x_n - x}{L_p}\right)$ Snp(x)= prexp(xp+) of excus Pno (arrivy Ppo xn -xp 0

Summary 13 R Va (jg(5) $\Delta p = \rho_{no} \exp\left(\frac{V_{\alpha}}{V_{\tau}} - 1\right)$ (a) An = npo exp(Ve-1) (a) of excess carriers. From figa, we see exponential decay of excess carriers in n and p regions. exp (va $A_n = n_{po}$ $\Delta p \approx P_{no} \left(e \times p \left(\frac{V_q}{V_T} \right) - 1 \right)$ exceps t's exass hole on on p-side n-sîde Ln & Lp - Diffusion length of e and holes. (- plengtn over which holes/e-s travels by dibbusion before it recombines) 1. Va=VF(F.B) lowers built -in potential barrier, so that e from n-segion are injected into pregion, oceating excess minority carriers in progion. These excess carriers (es) begin diffusing into boly pregion, where they can secondine with majority corrier holes. , The excess minority carrier (e) concentration then Ises with distance from the junction.

We know,

$$\int dp_{n}(x) = p_{n}(x) - p_{n}(x)$$
(Assumption: Uniformly deped regions, thurned equilibrium)

$$\int d(dr_{n}(x)) = d(h(x)) - d(P_{n})$$

$$= d(f_{n}(x)) = d(P_{n}(x)) - (x)$$

$$\int d(dr_{n}(x)) = d(P_{n}(x)) - (x)$$

$$\int d(dr_{n}(x)) = d(P_{n}(x)) - (x)$$

$$\int p(x_{n}) = -q Dp \frac{d(dr_{n}(x))}{dx} \int_{x=x_{n}} (Forn - 2)$$

$$\int d(dr_{n}(x)) = f_{n} \int e^{x_{n}} p \int_{x=x_{n}} (Forn - 2)$$

$$\int d(dr_{n}(x)) = f_{n} \int e^{x_{n}} p \int_{x=x_{n}} (Forn - 2)$$

$$\int d(dr_{n}(x)) = f_{n} \int e^{x_{n}} p \int_{x=x_{n}} (Forn - 2)$$

$$\int d(dr_{n}(x)) = f_{n} \int e^{x_{n}} p \int_{x=x_{n}} (Forn - 2) \int_{x=x_{$$

Similarly, at
$$x = xp$$
, e^{-} differsion curvest durity f_{1}
 $f_{1}(x) = \frac{1}{2}D^{-}\frac{1}{2}\frac{1}{2}d_{2}\int_{x=xp}$
 $f_{2}(x) = \frac{1}{2}D^{-}\frac{1}{2}\frac{1}{2}d_{2}\int_{x=xp}$
 $f_{2}(x) = \frac{1}{2}D^{-}\frac{1}{2}\frac{1}{2}D^{-}\frac{1}{2}d_{2}\int_{x=xp}$
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 $f_{2}(x) = \frac{1}{2}D^{-}\frac{1}{2}D^{-}\frac{1}{2}D^{-}\frac{1}{2}d_{2}\int_{x=xp}$
 $f_{2}(x) = \frac{1}{2}D^{-}\frac{1}{2}$

where, $I_0 = \left[\frac{2AD_{P.Pno}}{L_P} + \frac{2AD_{n.NPO}}{L_n}\right]$ 17 Io - Reverse saturation curvent $ie \left| I = I_0 \left[exp\left(\frac{V_a}{V_T} \right) - 1 \right] \right|$ ie Furnand - bias voltage ___ Va fig 6: Ideal I-V characteristic of a pr junction did . If the voltage Va becomes regative (severse -bias), ie If Va=-VR then $I = -I_0$ $\left\{ exp\left(\frac{longe}{r_{oduc}} \right) = 0 \right\}$ ie Current saturates to Io in the negative direction and it is independent of voltage (applied severse bias) ". To is referred to as "reverse saturation current." **INDERJIT SINGH**

1. Find receive solucidion curvent in a Si prijenction
1. Find receive solucidion curvent in a Si prijenction
13. The solution of the following parameters
Na, Nd = 10¹⁰ (m³),
$$Dr = 25 \text{ and } 3$$
, $Dr = 10 \text{ and } 3$,
 $TP = Tn = 5 \times 10^{-3}$, $On = 25 \text{ and } 3$, $Dr = 10 \text{ and } 3$,
 $TP = Tn = 5 \times 10^{-3}$, $On = 25 \text{ and } 3$, $Dr = 10 \text{ and } 3$,
 $TP = Tn = 5 \times 10^{-3}$, $On = 25 \text{ and } 5$, $Dr = 10 \text{ and } 3$,
 $Solphi To = 2A \left[\frac{Dr}{Tr} \text{ from and bias } + 0.65 \text{ V and } A + course watered
 $A + course \text{ watered in a set of 100}$.
 $Solphi To = 2A \left[\frac{Dr}{Tr} \text{ from and } n_{PD} = \frac{n^{-2}}{Rm} + \frac{n^{-2}}{Mm}\right]$
 $We Know, Rno = \frac{n^{-2}}{n_{no}} \approx \frac{n^{-2}}{Na}$ and $n_{PD} = \frac{n^{-2}}{Rm} \approx \frac{n^{-2}}{Na}$.
 $L^2 = DnTr \Rightarrow Lr = \sqrt{DrTr} \approx 2.236 \times 10^{-3} \text{ cm}$.
 $L^2 = DnTn \Rightarrow Ln = \sqrt{DnTn} \approx 3.535 \times 10^{-3} \text{ cm}$.
 $L^2 = DnTn \Rightarrow Ln = \sqrt{DnTn} \approx 3.535 \times 10^{-3} \text{ cm}$.
 $L^2 = 1.6 \times 10^{-16} \left[11.54 \text{ km}^2\right]$
 $To = 1.6 \times 10^{-16} \left[11.54 \text{ km}^2\right]$
 $T = 3.6 \times 10^{-16} \left[11.54 \text{ km}^2\right]$
 $T = 10 \left[\exp\left(\frac{N/2}{(0.025)}\right]^{-1}\right]$
 $L = 0.323 \text{ mA}$
 $V_{free} V_{fee} = 0.65 \text{V}$
HOHIS THURSDIM$

112 68 69

So five, we derived

$$J_{P}(x_{n}) = \frac{q \operatorname{De} p_{n}}{L_{P}} \left[e_{P}(\frac{v_{n}}{v_{r}})^{-1} \right] \longrightarrow \operatorname{Minority}_{derives at the edge of the service of distance through for a sequence of the service of th$$

20. Ð Θ P 0 Θ Ð Pr junction . in Forward bias $\Delta \rho = \rho_{no}\left(ex\rho\left(\frac{Va}{VT}\right)-1\right) = \rho_{no}\left(e^{\left(\frac{Va}{VT}\right)}-1\right)$ $\Delta n = n \rho_0 \left(e^{\left(\frac{\sqrt{a}}{\sqrt{r}} \right)} \right)$ a) Concrof Cxuss carviers +Ln stp-A Current density is constant -Tr Jndnift Jpdnift Jpdnift & Jodnif b) Ideal e and hole Jp(xn) to doibt current components Jn(-xp) Indibb Jpdibb through a pr jurch + Jadily & Jpdilt under forward big due to dibbusio -xp 2=0 2n Points to Remember: (from (a) and (b) diagram) ie [pn Junch in forward bias] 1. Excuss minosity carrier decay exponentially in n and p segions (from (a)). Total current in a prijurction is constant (from (b)) 2. Majority carrier current flow beaz of -3. Minosity carrier current flow is kecor of -> (Jndigt, Jpdibt). -> 4.

1. An Si abapt on junction with
$$A = 10^{-4} \text{ cm}^{2}$$
 has following. 21
properties at 300%.
 $P = 3^{-1} \text{ cm}^{-1}$ nside
 $Na = 10^{-1} \text{ cm}^{-3}$ $Nd = 10^{-2} \text{ cm}^{-3}$
 $Tn = 0.1 \text{ sase}$ $Tr = 10 \text{ sase}$
 $Ap = 200 \text{ cm}^{-1} \text{ lss}$ $Tr = 10 \text{ sase}$
 $Ap = 200 \text{ cm}^{-1} \text{ lss}$ $Tr = 10 \text{ sase}$
 $Ap = 200 \text{ cm}^{-1} \text{ lss}$ $Tr = 10 \text{ sase}$
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 $Ap = 200 \text{ cm}^{-1} \text{ lss}$ $Tr = 10 \text{ sase}$
 $Tr = 10 \text{ sase}$ $Tr = 10 \text{ sase}$ $Tr = 10 \text{ sase}$ $Tr = 100 \text{ sase}$ $Tr = 100 \text{ sase}$
 $Tr = 90 \text{ cm}^{-2} \text{ sase}^{-2} \text{ sase}^{-2} \text{ (}15 \text{ sase}^{-2} \text{ sase}^$